



Energy research Centre of the Netherlands

## Stabilised Waste - Cement barrier - Soil interfaces

Hans van der Sloot, Hans Meeussen, Paul Seignette, Josh Arnold, David Kosson  
ECN, Netherlands  
Vanderbilt University, Nashville



## OVERVIEW

Problem definition

Release of non-interacting species (3 layer model)

Scale issues

Illustration of detailed chemistry

Chemistry of individual layers

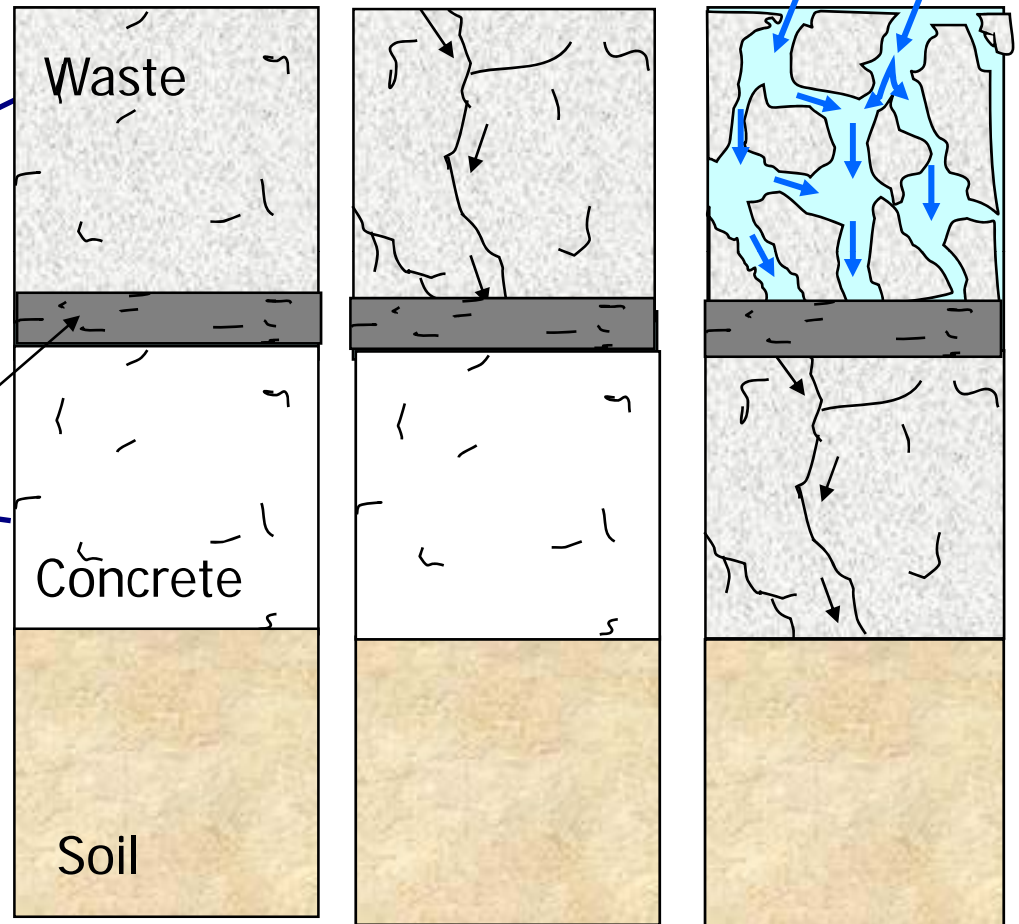
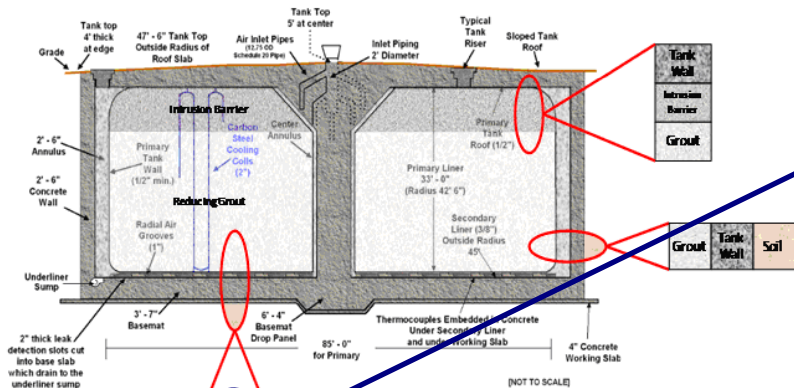
Interface reactions (diffusion in 3 layer model)

Carbonation and uncertainty

Conclusions

## POSSIBLE CHANGES IN THE TANK CLOSURE SYSTEM AT LONG TERM

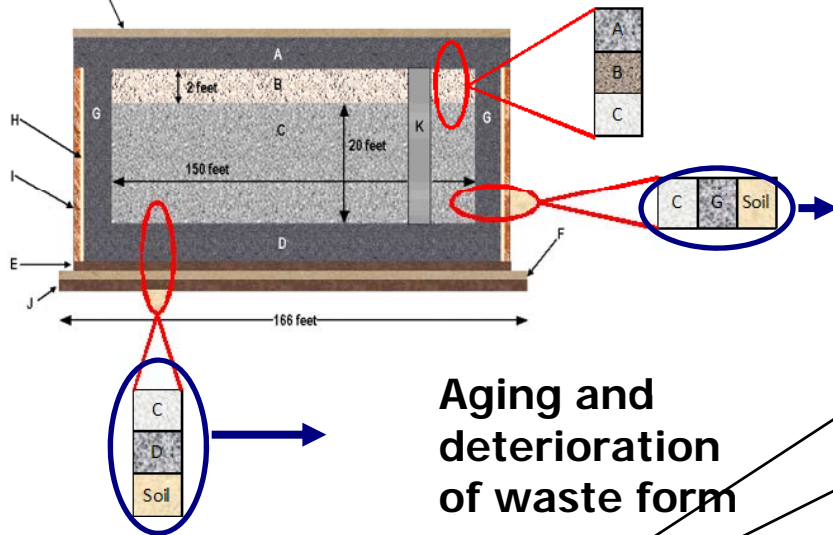
### TANK CLOSURE



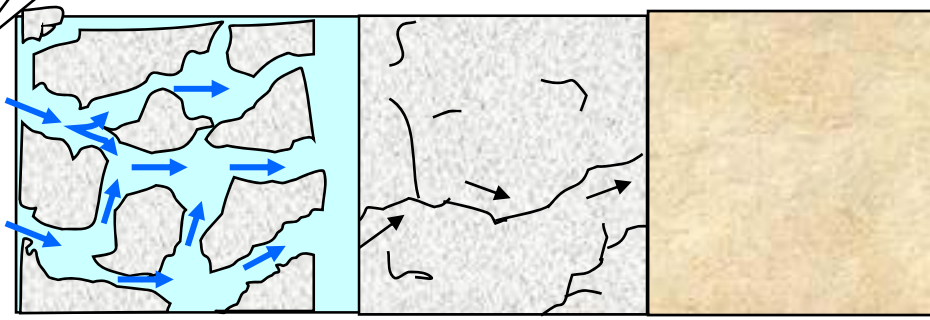
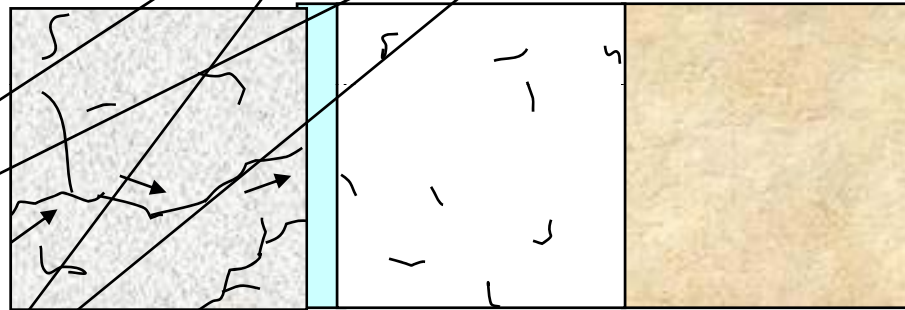
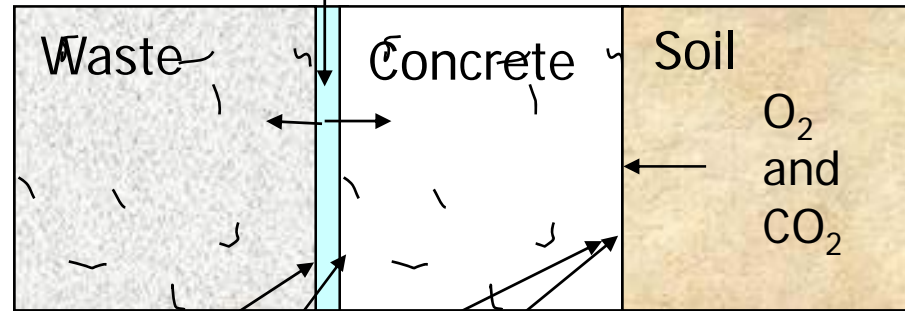
Aging and deterioration of waste form

O<sub>2</sub> and CO<sub>2</sub>

## LL WASTE VAULT

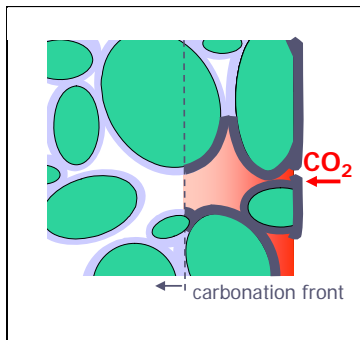


**Aging and deterioration of waste form**

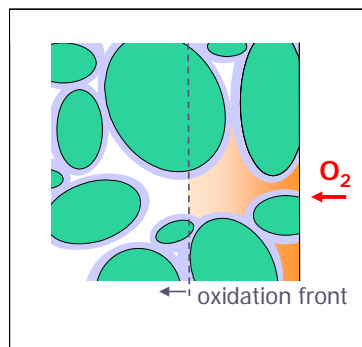


Air void (partially water filled?)

### Carbonation

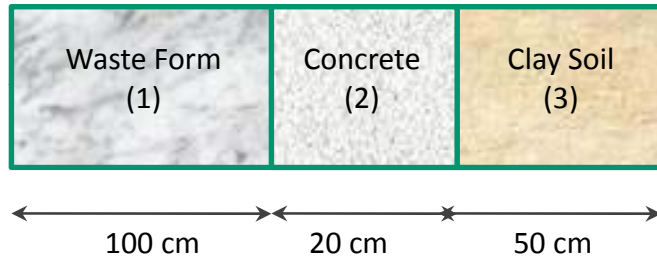


### Oxidation



## Effect of Boundary Conditions and Saturation on Release from a 3-layer System

3-Layer, 1-D diffusion model for non-interacting, conservative species (e.g., Na)



	Waste Form	Concrete	Clay Soil (compacted)
Density (g/cm <sup>3</sup> )	1.7	2.4	1.8
Porosity	0.4	0.1	0.35
Tortuosity (sat'd)	5	15	2

### Boundary Conditions

Waste form – no flux at interior boundary (left side)  
Clay soil – zero concentration at external boundary (right side of clay soil)

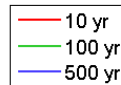
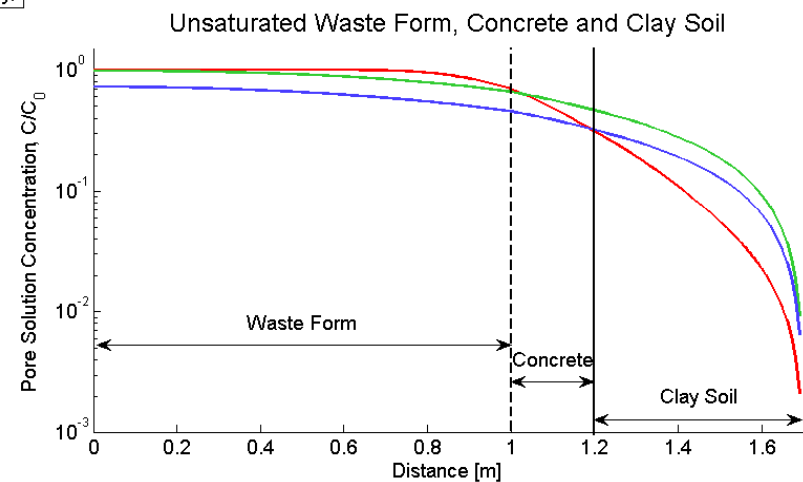
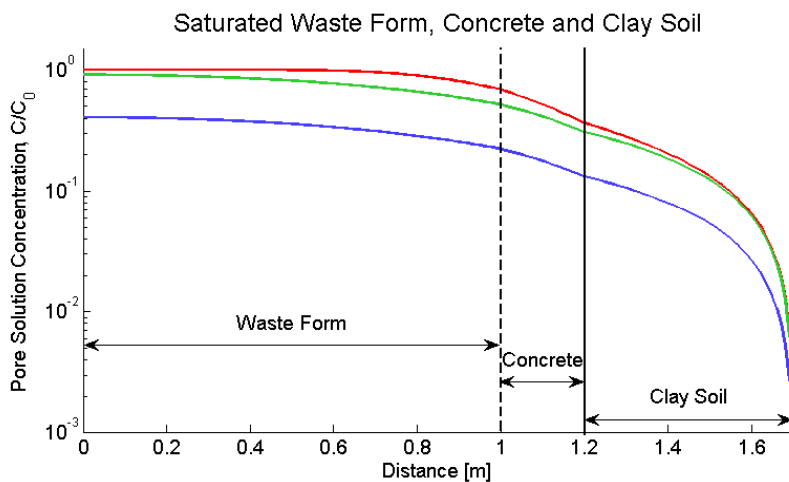
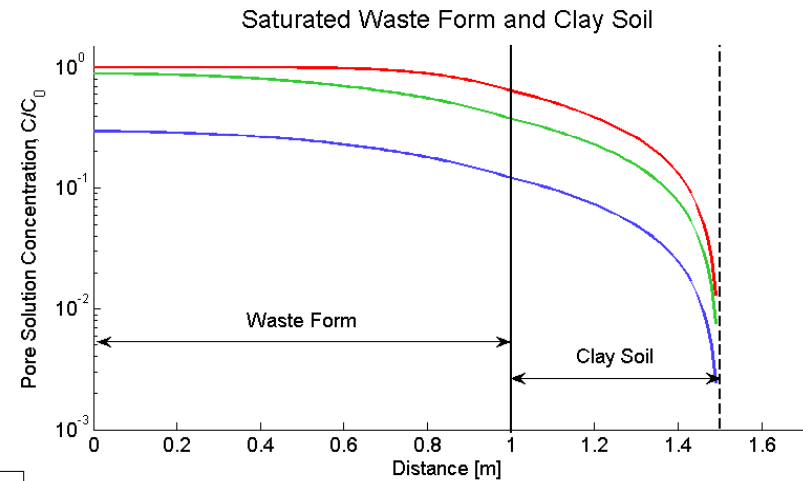
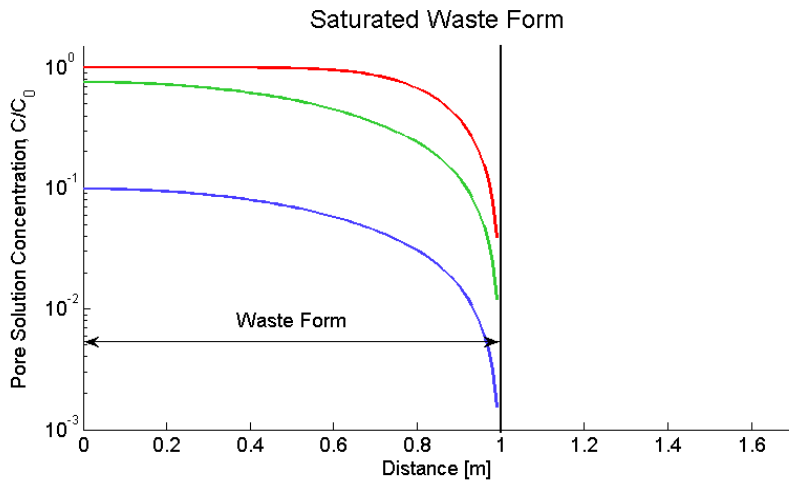
### Initial Condition

Na only in waste form at time zero at  $C/C_0=1$

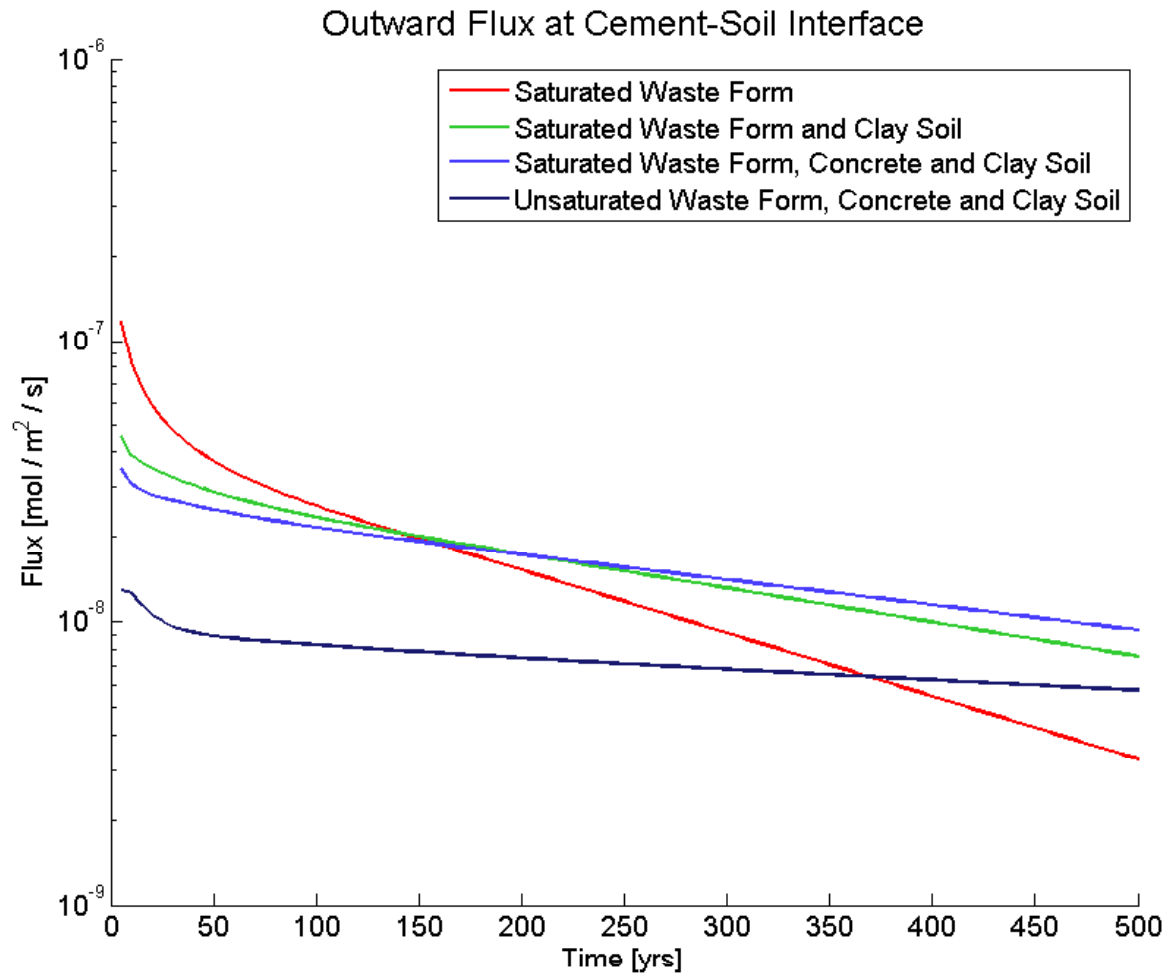
### Cases

1. Saturated
2. Unsaturated (tortuosity values assumed 2x for both waste form and concrete and 3.2x for soil; available porosity assumed 0.8x for waste form and concrete and 0.16 x for soil)
3. Same as (1) but with concrete layer only and  $C/C_0=1$  at waste form-concrete interface and  $C/C_0=0$  at concrete-clay soil interface
4. Same as (1) but with waste form only and  $C/C_0=0$  at waste form boundary (waste form in infinite bath)

## Transport of non-interacting species in 1-, 2-, and 3-layer system (sat – unsat)

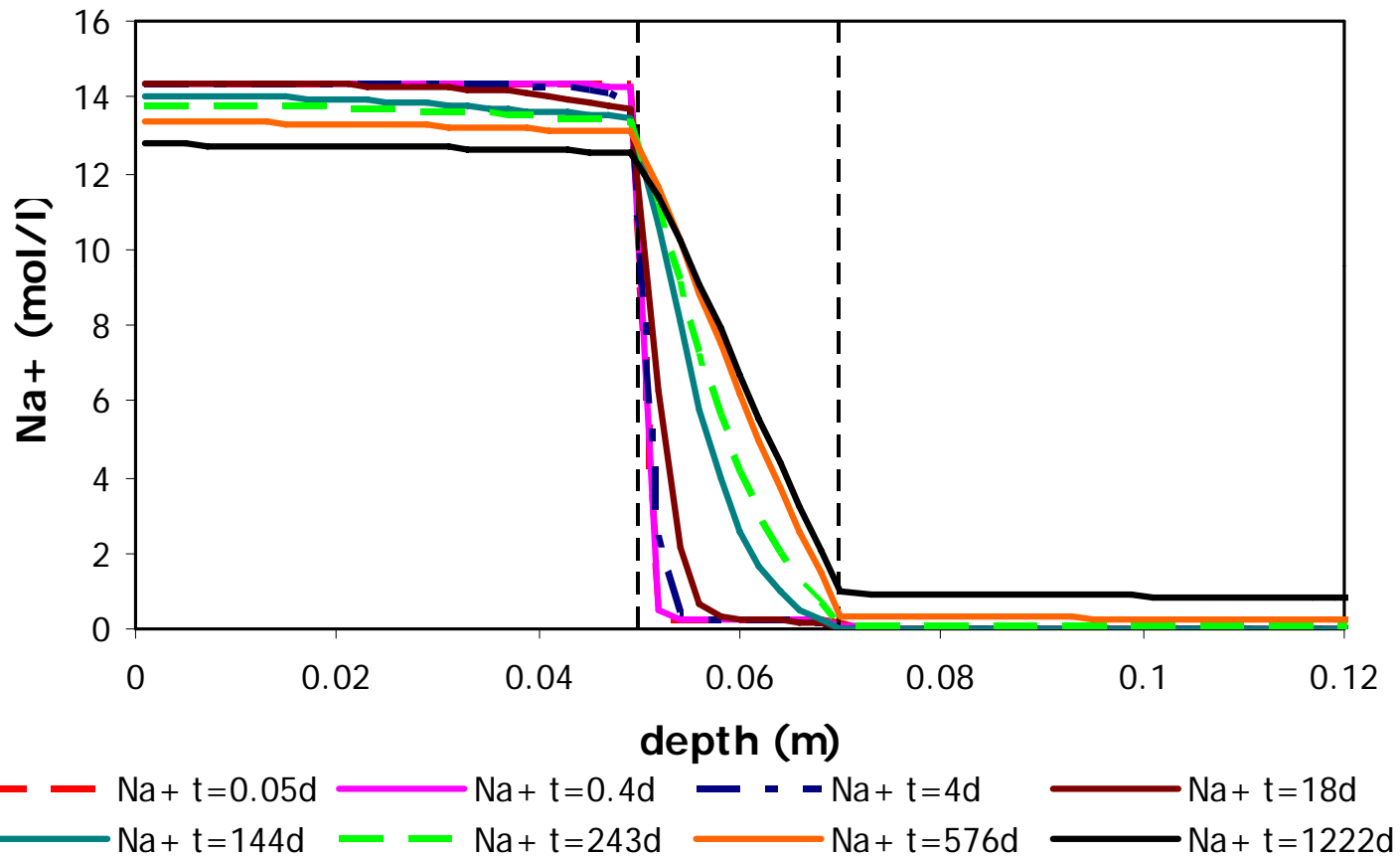


## Flux of non-interacting species at the cement-soil interface



## Scaling to smaller dimensions with same physical conditions

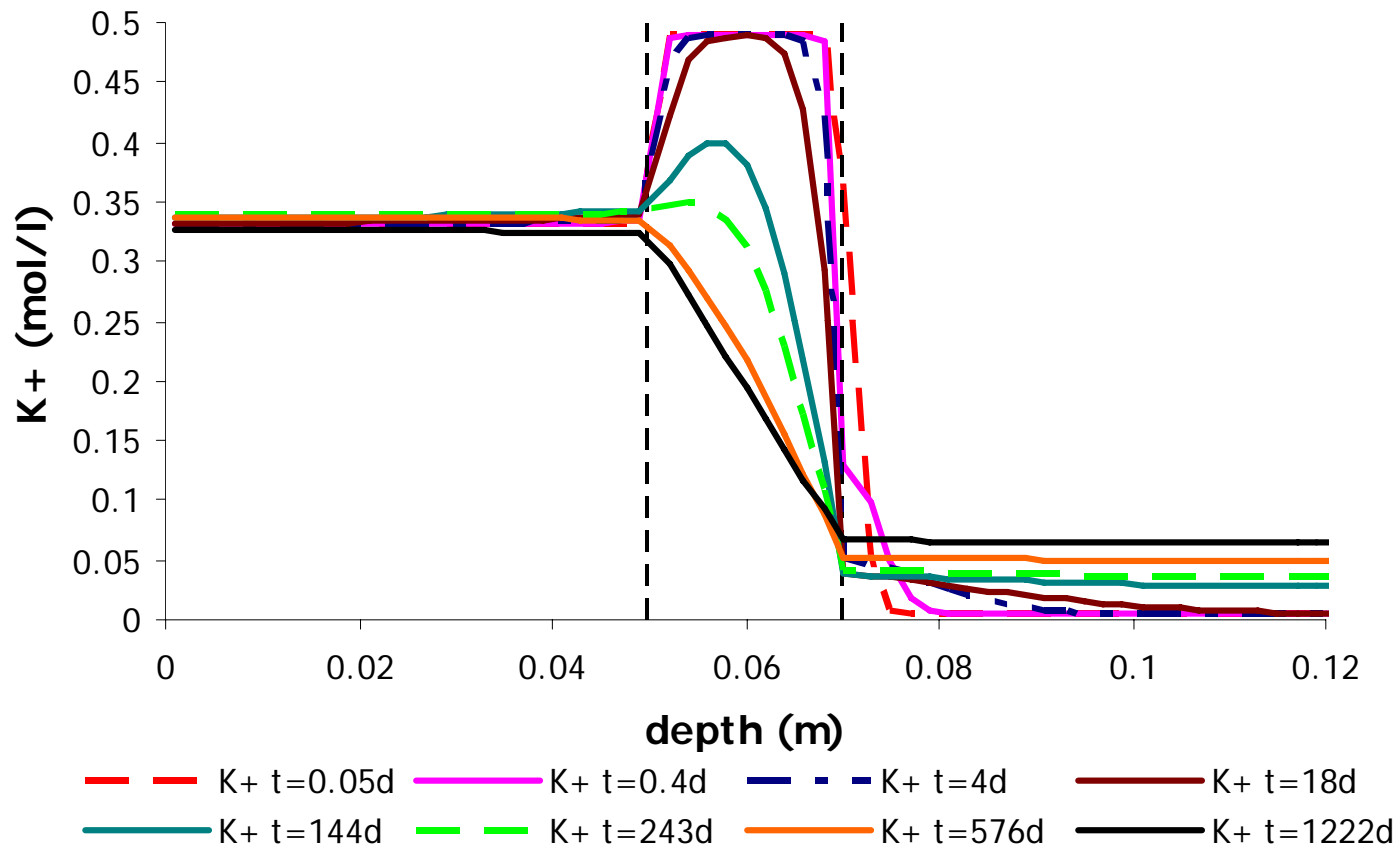
Na<sup>+</sup> release from a waste through a cementitious barrier into a clayey soil



Steady state condition established within 2 years



### K<sup>+</sup> release from a waste through a cementitious barrier into a clayey soil



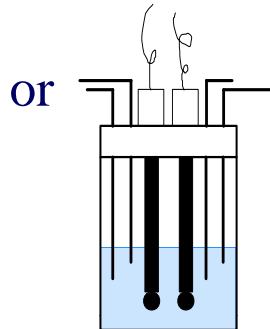
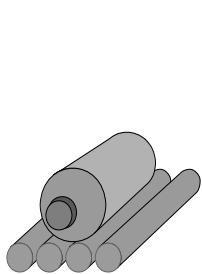
In spite of higher K level in barrier steady state condition established within 2 years

## Illustration of the importance of more detailed chemistry

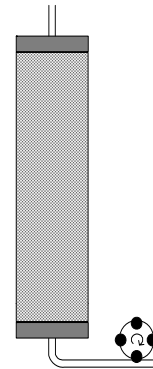
Geochemical speciation modeling based on pH dependence test results taking mineral precipitation, clay interaction, sorption on ironoxides, incorporation in ettringite and interaction with particulate and dissolved organic matter into account.

Sorption parameters for particulate and dissolved organic matter for U and Th based on the generic parameters derived by Milne et al, 2003 for the Nica Donnan model.

## GRANULAR MATERIALS



**pH DEPENDENCE TEST: BATCH MODE**  
 ANC, CEN/TS 14429,  
 or EPA method 1313  
 or, COMPUTER CONTROLLED CEN/TS 14997



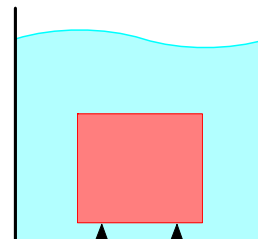
**PERCOLATION LEACHING TEST**  
 CEN TS 14405 or  
 EPA method 1314

Standardisation:  
 CEN/TC292, ISO/TC190,  
 CEN/TC345, CEN/TC351,  
 SW846

## MONOLITHIC MATERIALS

**Same as granular**

+

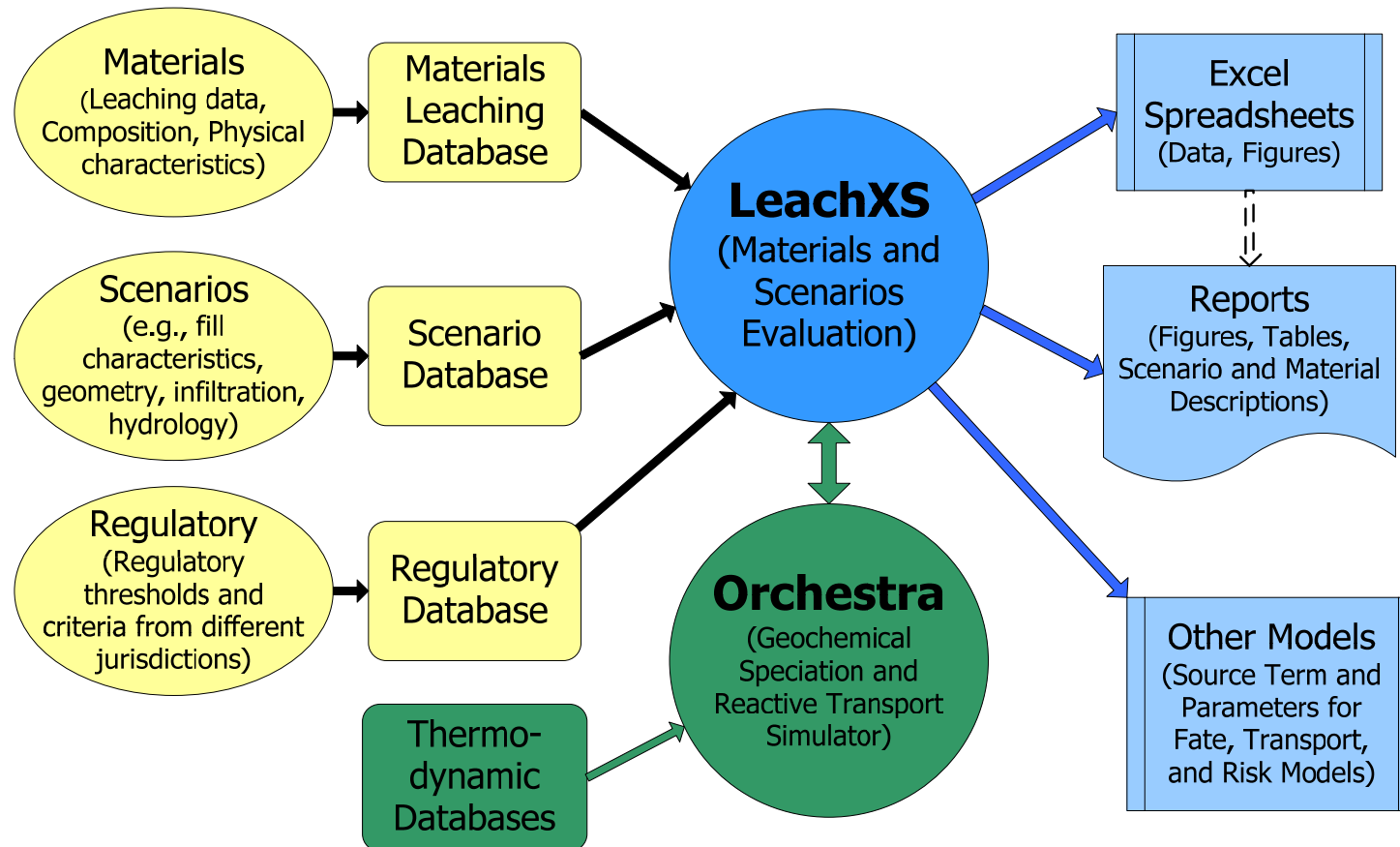


**TANK LEACH TEST MONOLITH** CEN/TS 15863 and EPA method 1315 and **COMPACTED GRANULAR LEACH TEST** (NEN 7347 and EPA method 1313).

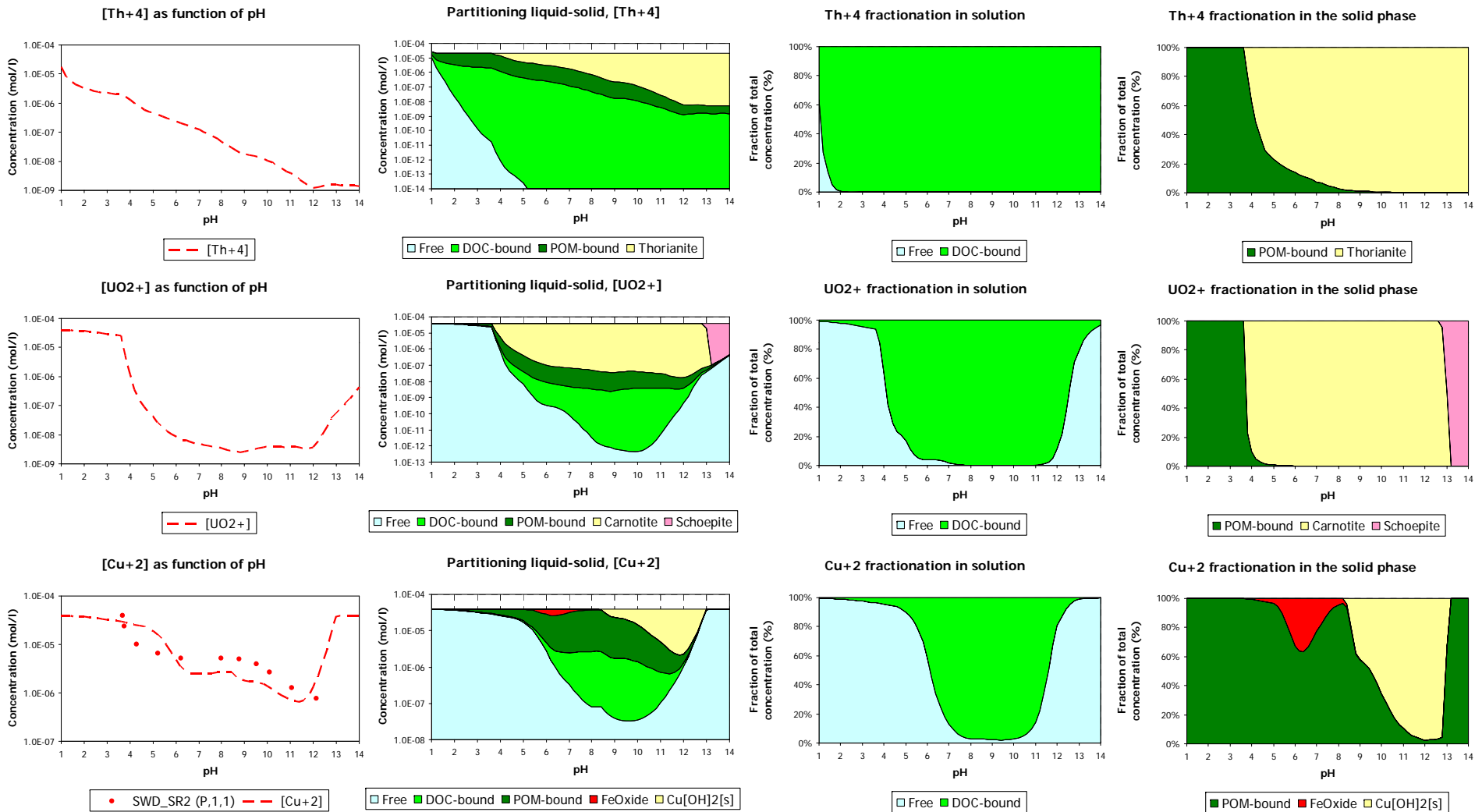
Chemical speciation aspects

Time dependent aspects of release

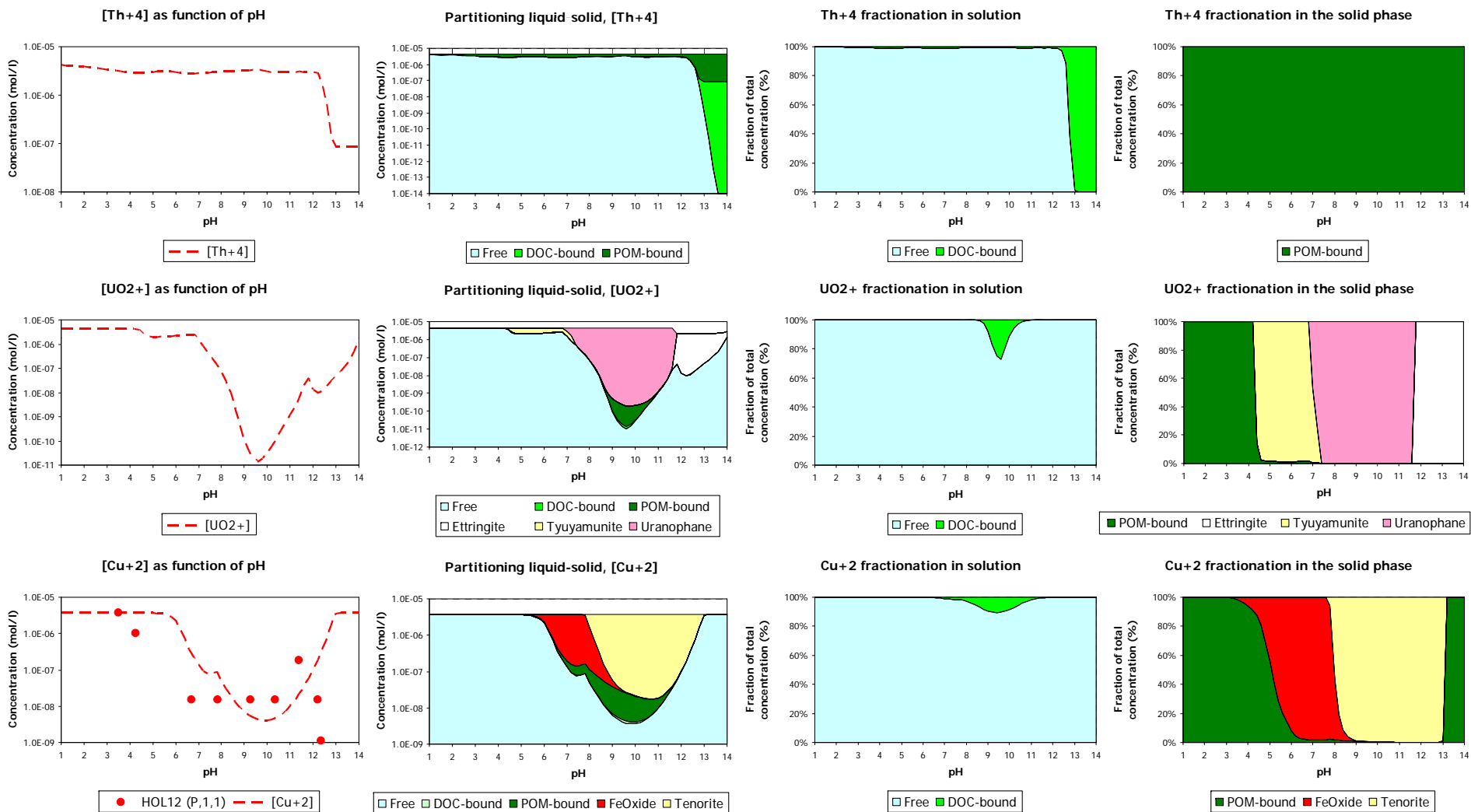
## LeachXS Structure



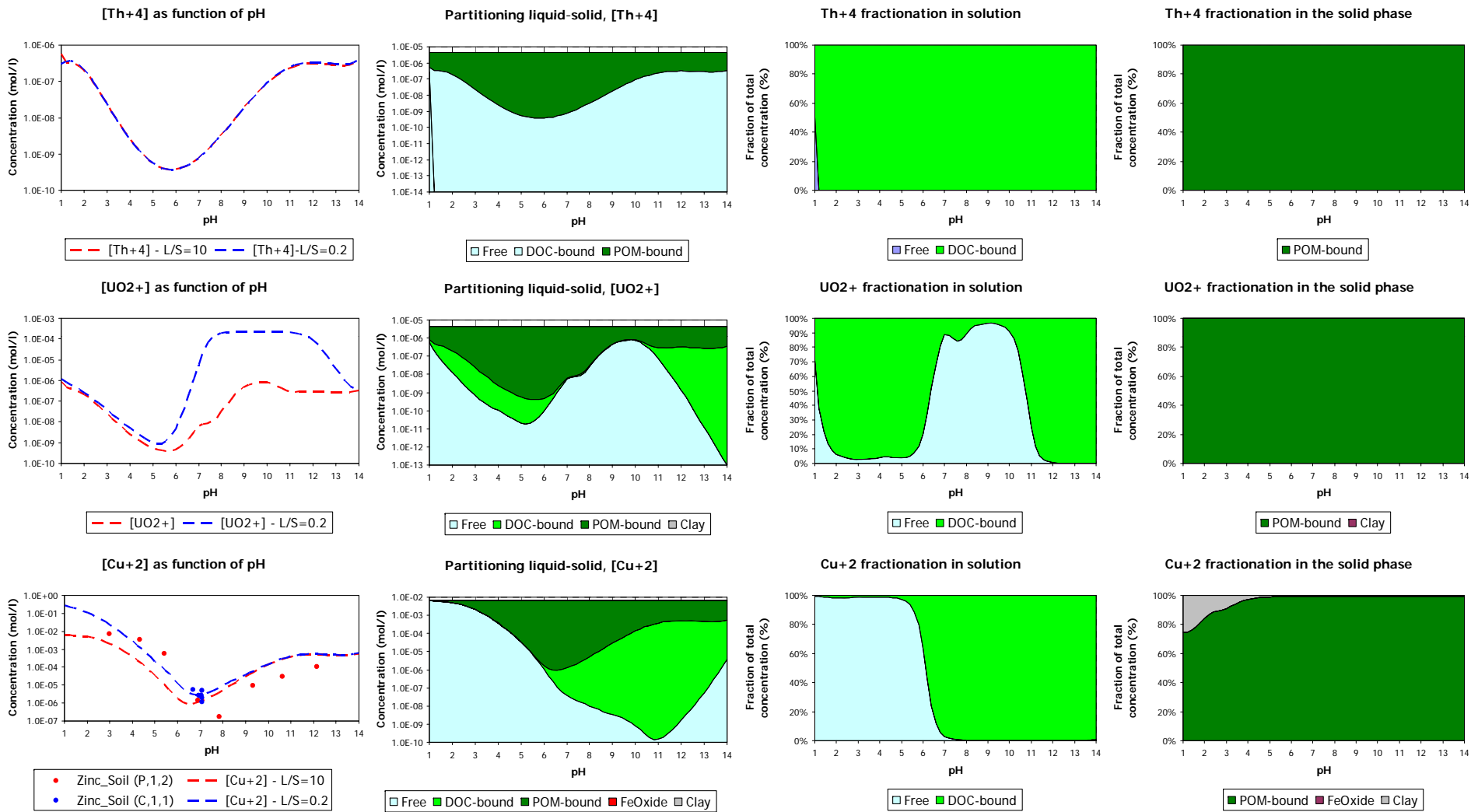
In the modeling mineral dissolution, sorption on hydrated ironoxides, clay interaction, interaction with particulate and dissolved organic matter and incorporation in ettringite solid solution.



Information also relevant for stabilisation of contaminated soil



Cement mortars and concrete not inorganic: non-negligible organic matter content!



Soil system dominated by dissolved and particulate organic matter interaction

## Input specification

**Diffusion Case** Stabilised Waste - CEM II GBFS-FA - Soil OXIDISED/ CARBONATED  
**Layer overview**

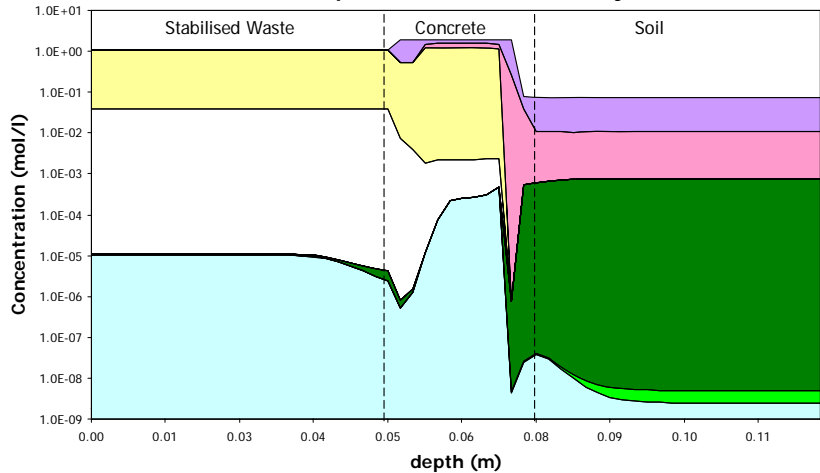
<b>Material</b>	Stabilised waste	GBFS-FA-Mortar	Soil
<b>Length</b>	5.00	2.00	5.00 <b>cm</b>
<b>Porosity frc</b>	0.40	0.10	0.35
<b>Tortuosity</b>	3.00	10.00	2.00
<b>Density</b>	1.70	2.40	1.70 <b>kg/dm<sup>3</sup></b>
<b>pH</b>	10.1	11.5	6.5
<b>pe</b>	15	15	15

In the modeling mineral dissolution, sorption on hydrated ironoxides, clay interaction, interaction with particulate and dissolved organic matter and incorporation in ettringite solid solution.

Typically 44100 variables, 192565 expressions, 118 equations

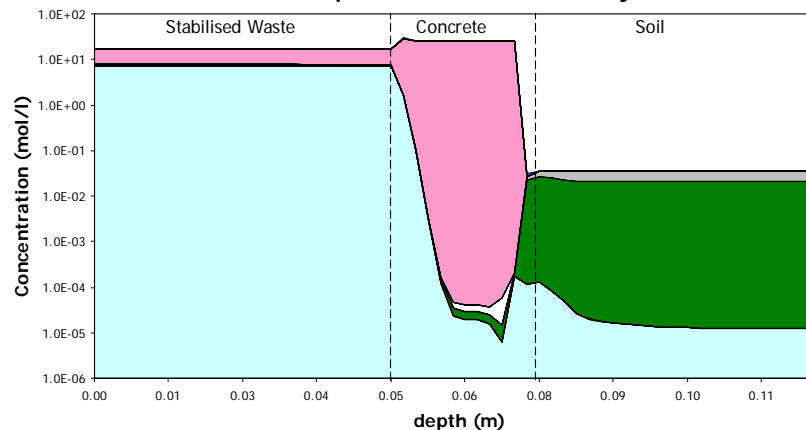


Distribution profile for Al<sup>3+</sup> after 6 days



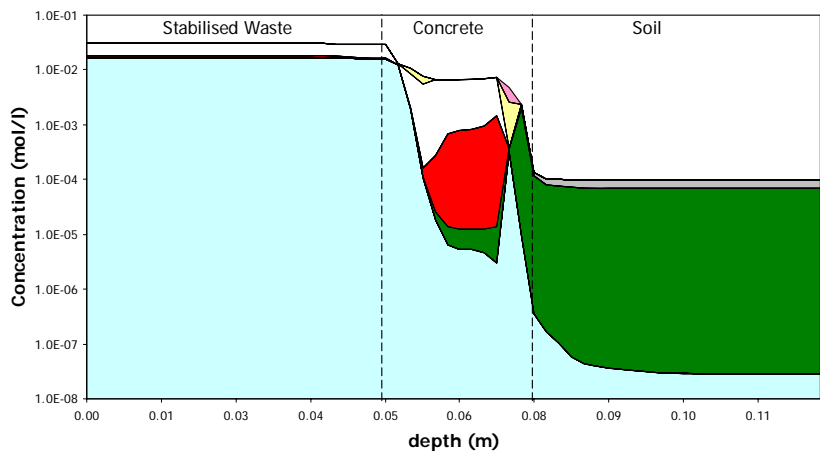
Free DOC-bound POM-bound Clay Ettringite AA\_Gibbsite Albite[low] Kaolinite

Distribution profile for Ca<sup>2+</sup> after 6 days



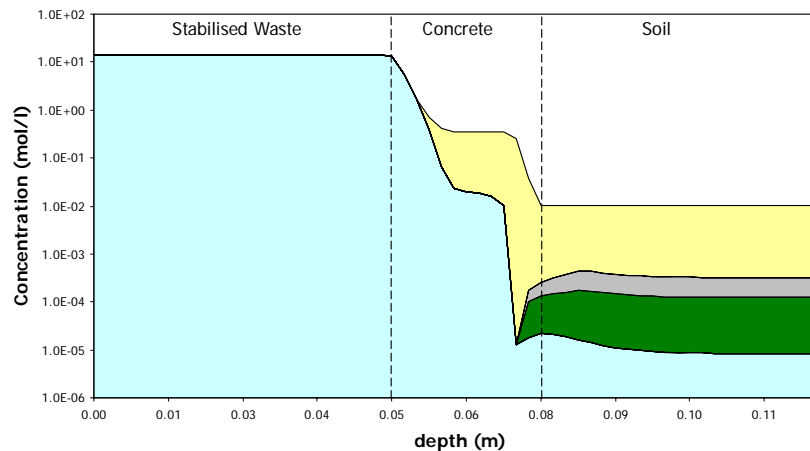
Free DOC-bound Clay AA\_2CaO\_Fe2O3\_SiO2\_8H2O[s] AA\_Calcite AA\_Gypsum

Distribution profile for Sr<sup>2+</sup> after 6 days

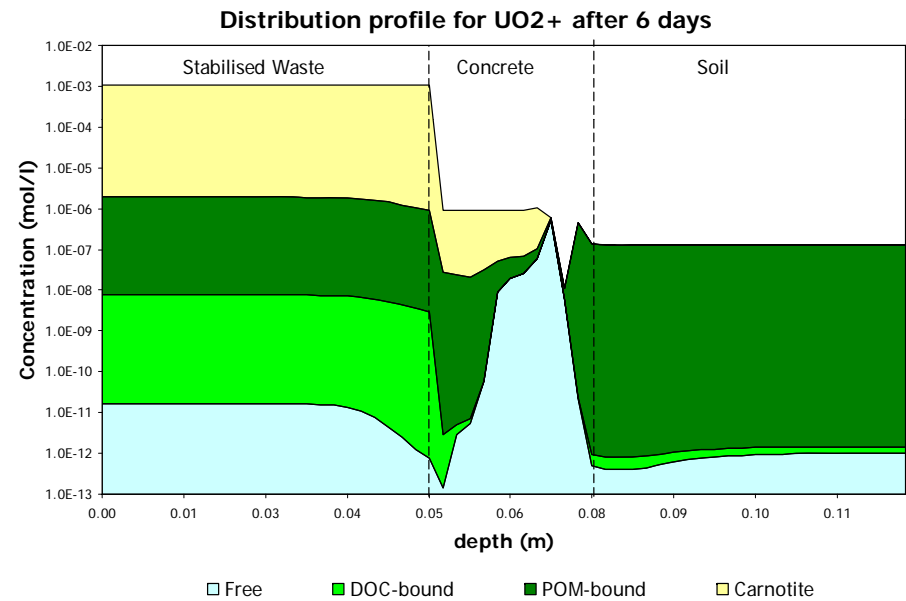
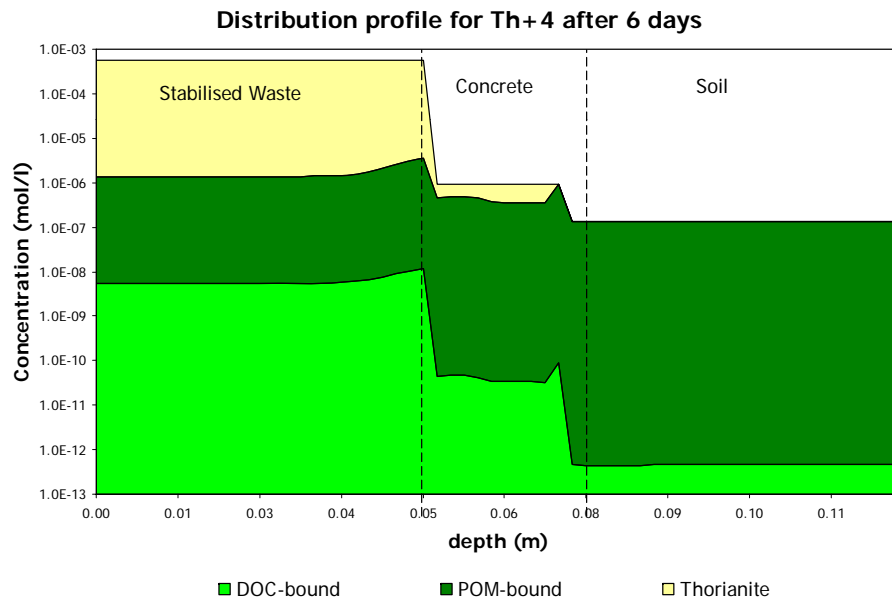


Free DOC-bound POM-bound FeOxide Clay Ettringite BaSrSO4[50%Ba] Strontianite

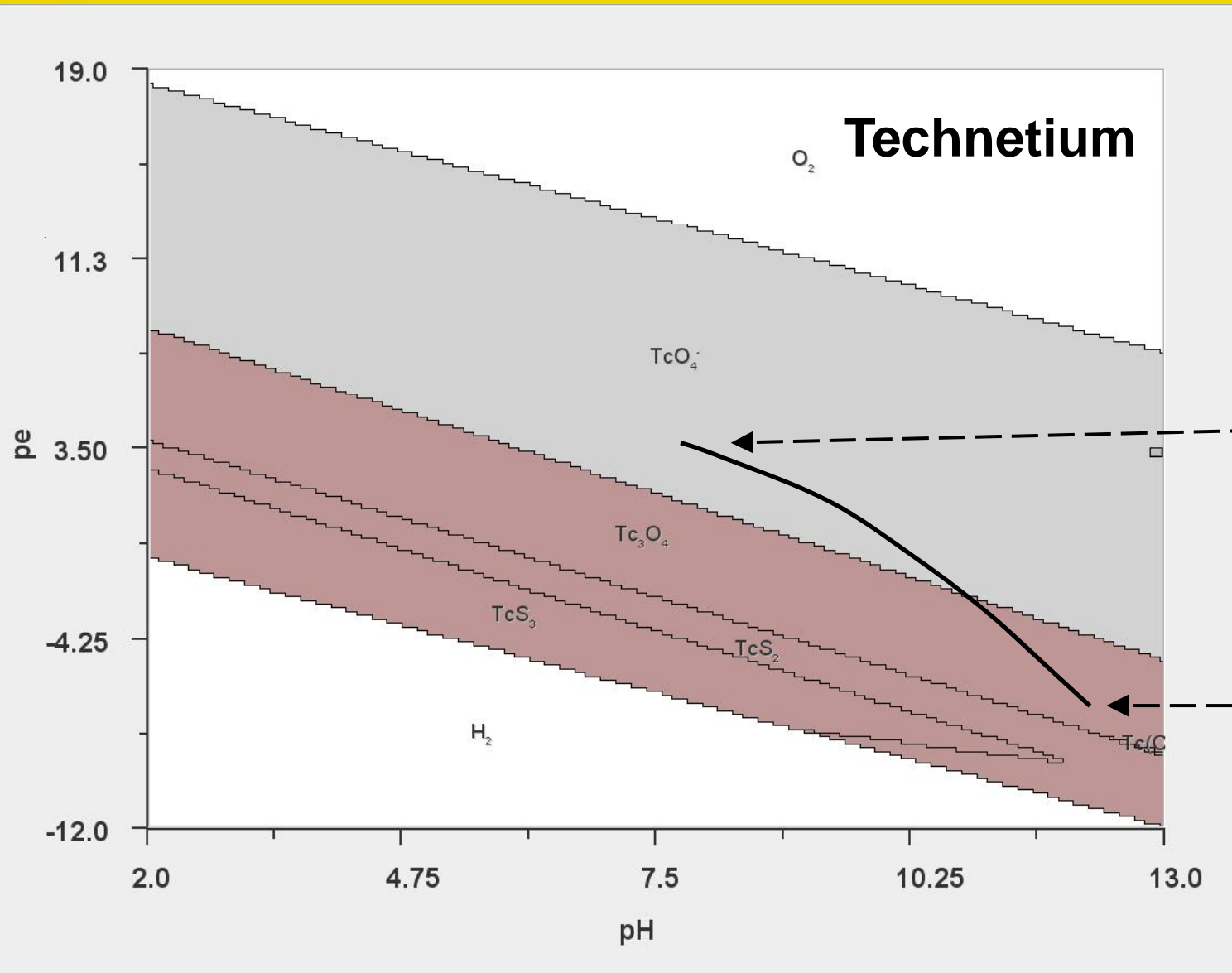
Distribution profile for Na<sup>+</sup> after 6 days



Free DOC-bound POM-bound Clay Albite[low]



Association with DOC important for release

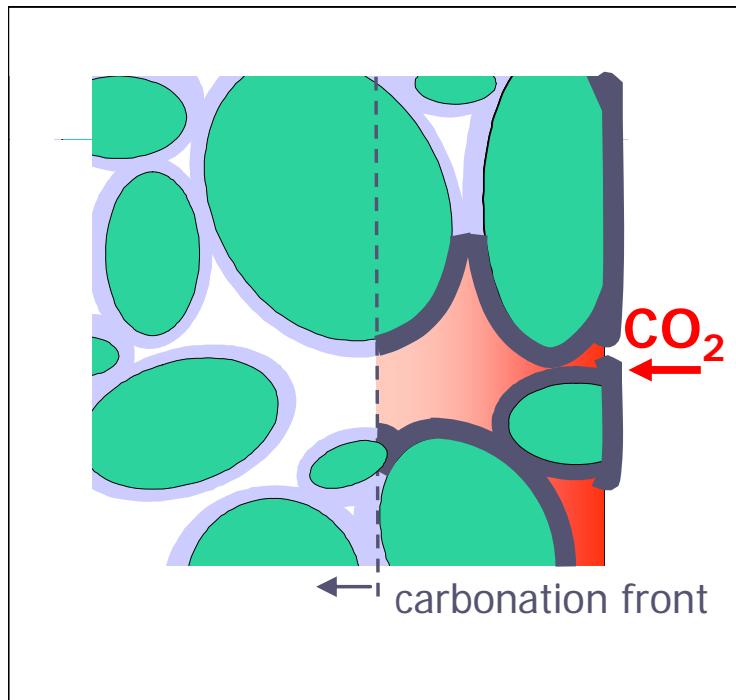


**Projected very long term condition – carbonated and oxidised**

**Initial condition – alkaline and reducing**

Carbonation leads to alterations in the release behaviour as a result of the pH change that is brought about

## Carbonation



The effect of carbonation on release is illustrated by modeling, including an evaluation of uncertainty in the model prediction.

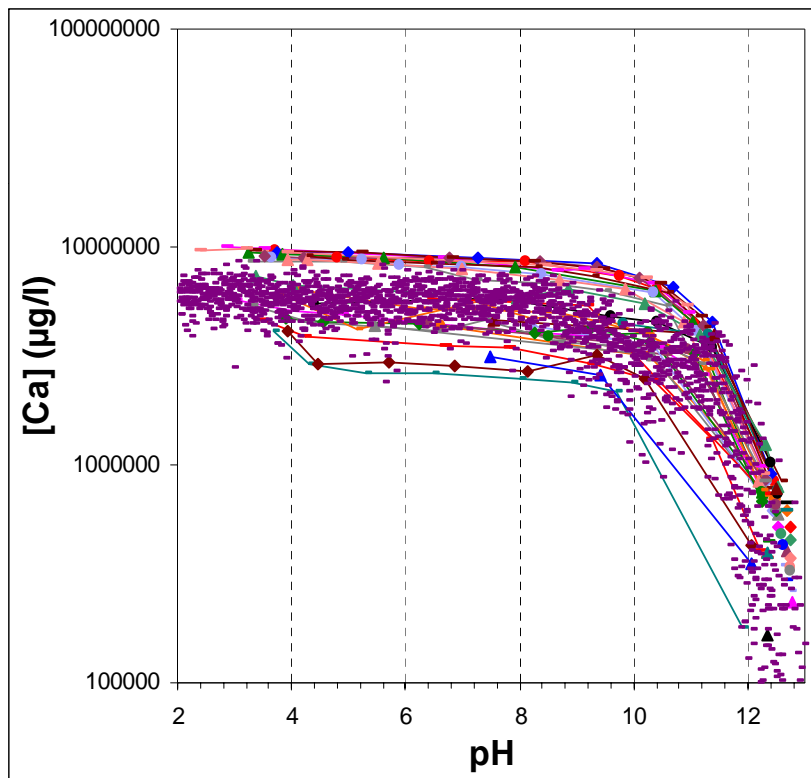
The data are placed in perspective to actually measured test data for > 70 different cement mortars (Portland as well as different types of blended cements)

## Stochastically varied input parameters for modeling of pH dependence leaching test data for cement mortars

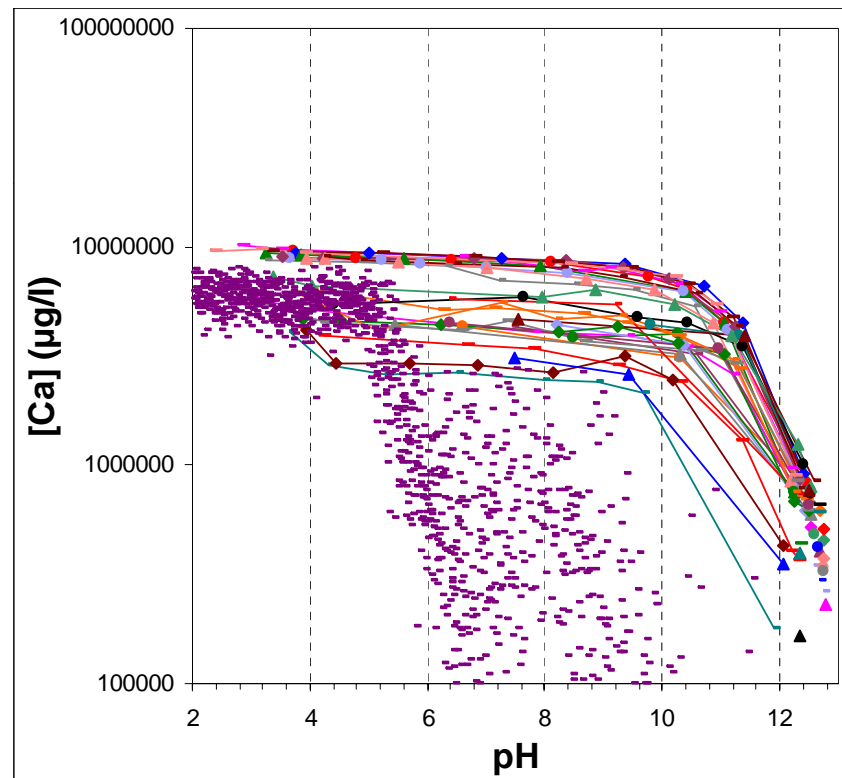
- Total available concentration (10%)
- pH (0.1 unit)
- Pe (2 units)
- All reaction constants (15%)
- Ionic strength (20%)
- Gaussian distribution
- 2000 simulations in the pH range 2-13

## Solubility of Ca in cement mortars as function of pH

### Without Carbonate

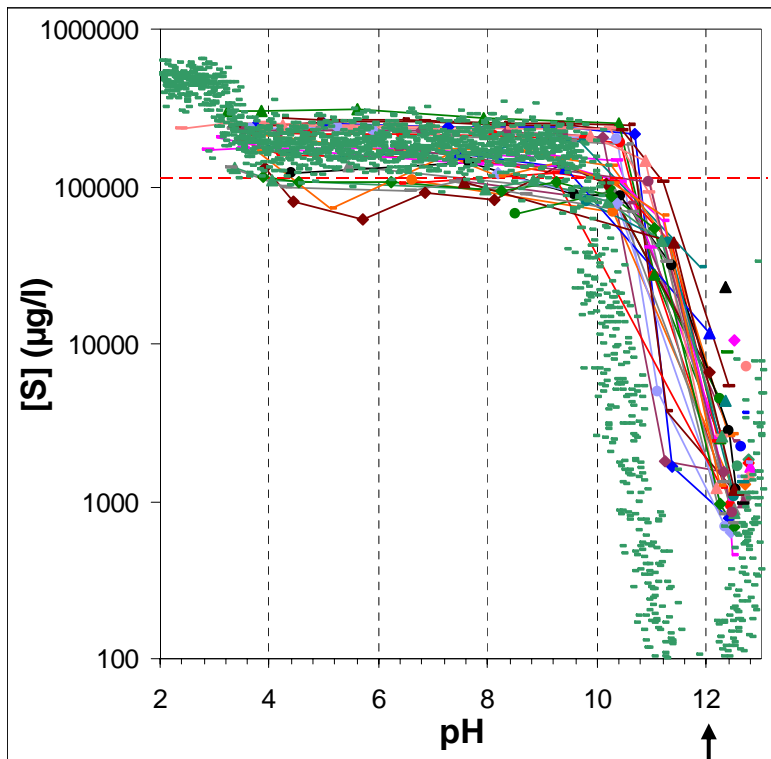


### With Carbonate



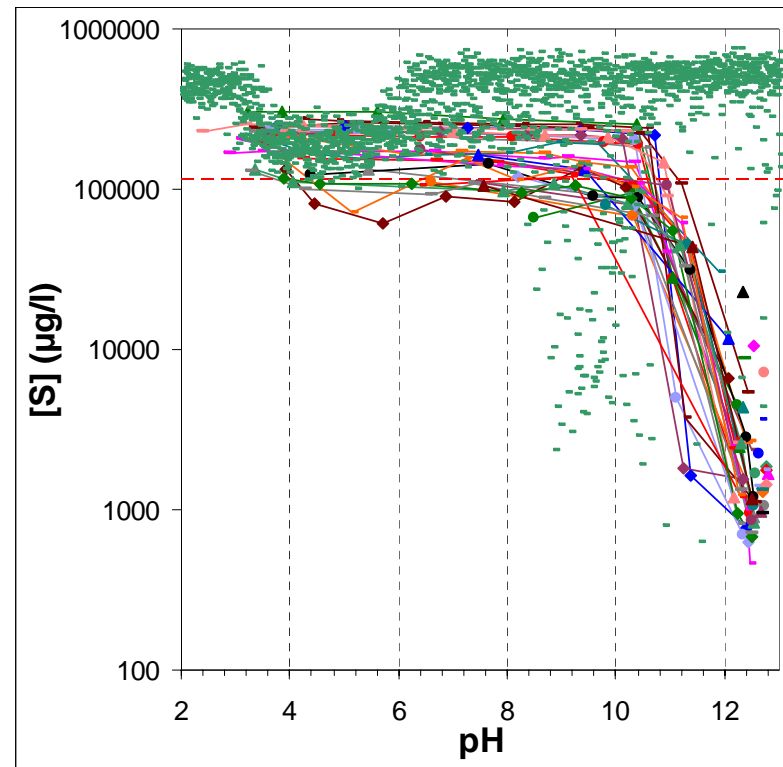
## Solubility of SO<sub>4</sub> as S in cement mortars as function of pH

### Without Carbonate



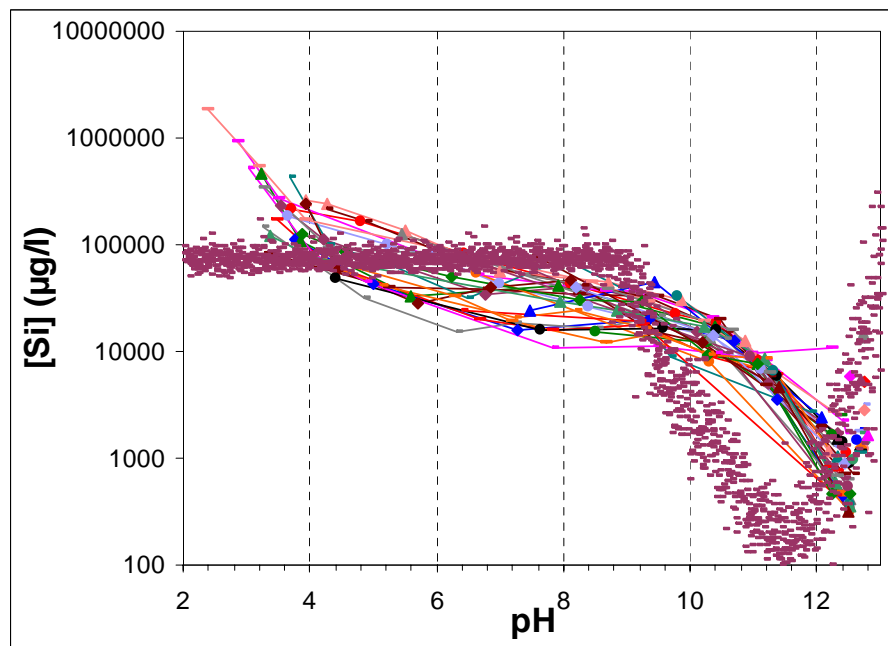
Ettringite

### With Carbonate

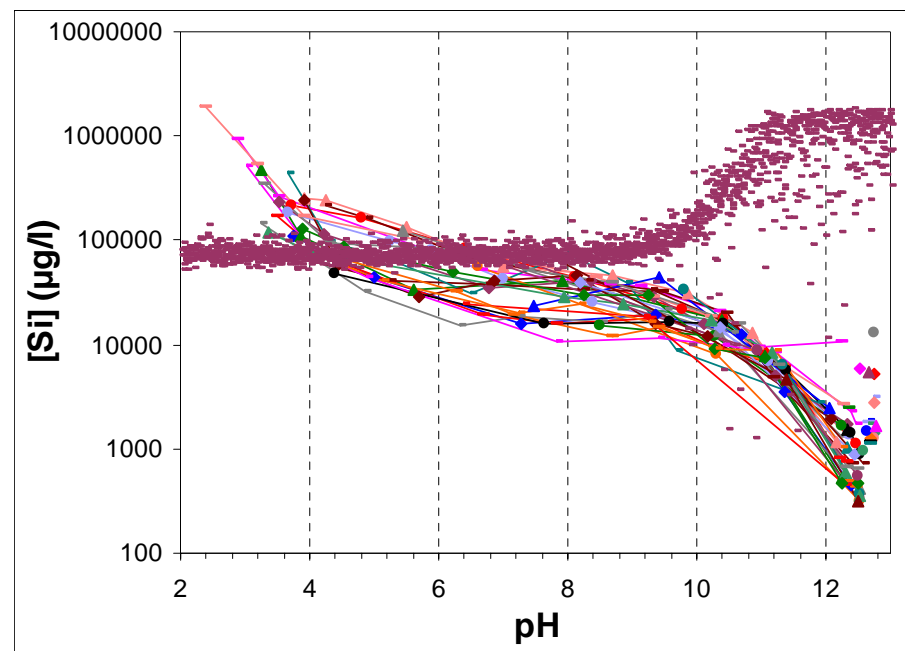


## Solubility of Si in cement mortars as function of pH

### Without Carbonate



### With Carbonate





## CONCLUSIONS

- Both physical and chemical changes in the waste form and cement barrier are of importance to properly assess release to the environmental.
- For non-reacting species a steady state condition of release through the barrier develops within a few years for saturated conditions. For unsaturated conditions this takes in the order of a hundred years.
- Carbonation and oxidation lead to important changes in release behaviour of substances. As these processes lead to moving fronts it is difficult to capture the release in a  $K_d$  describing contaminant behaviour of the entire waste form, the barrier or the soil.

## CONCLUSIONS

- Gaining insight in more detailed chemical interactions is of importance as mobilisation in the form of dissolved complexes may occur. Currently, organic matter interaction is not considered.
- The binding potential of hydrated ironoxide (formed in situ upon oxidation of reduced Fe in both waste and barrier) for radionuclides of interest is important for retention within the containment under oxidised/carbonated conditions.
- U and Th in the present model runs are preliminary and need further verification by measurement of actual release behaviour from size reduced stabilised waste. In case of U and Th, this is possible with stable isotopes. For Tc this is obviously not possible.
- Therefore, carrying out a pH dependence test on cement stabilised radioactive waste is highly recommended to provide better insight in release controlling processes.

## CONCLUSIONS

- More detailed chemical characterization provides the means to design for retention of contaminants in the waste or the design of a chemical barrier in addition to physical containment.
- Although calculation times with complex chemistry are long compared to  $K_d$  type calculations, it is possible to model release under defined conditions along the projected path as defined in a  $pe - pH$  diagram (resulting from carbonation and oxidation). More complete consideration of chemical processes also provides more robust understanding of non-linear process coupling and for improved design.
- Optimization of calculation efficiency. Balance complex models with simplified models. Preferably justified simplification based on understanding the underlying processes.